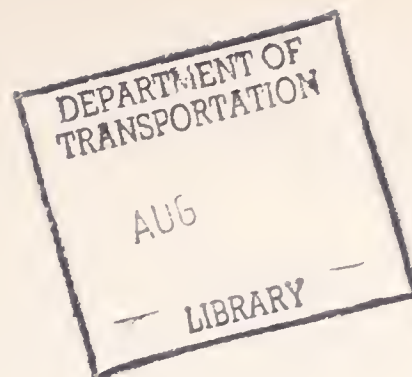


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U.S. Department
of Transportation
**National Highway
Traffic Safety
Administration**



DOT HS 807 275
Final Report

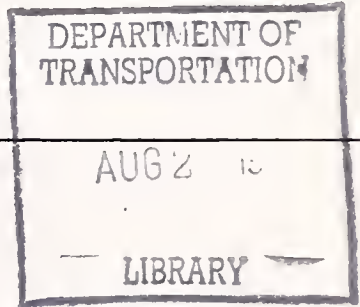
February 1988

Study of Differences in Hybrid III Chest Deflections Due to Three-and Two-Point Belt Loadings

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16. Abstract					
<p>Parametric studies were performed using the MVMA 2D crash victim simulation program to determine how chest deflection of two point and three point belt-restrained Hybrid III type dummies are affected by belt characteristics, seat cushion geometry and stiffness, floor board and knee cushion locations. Output parameters include hip motion, belt loads, chest deflection (top and bottom), knee loads, belt angles and chest g's. Results of the study indicate that chest deflection for comparable belt geometries are larger for two point belt systems than they are for three point belt systems, and that in all cases the deflection at the bottom of the chest when restrained by a two point belt system is significantly larger than at the top of the chest.</p>					
17. Key Words MVMA 2D, CVs, Hybrid III, Chest Deflection, Belt Restraints, Mathematical Modeling			18. Distribution Statement National Technical Information Service Springfield, VA		
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This letter describes the work that has been done under Order No. DTNH22-87-P-02088, "Study of Differences in Hybrid III Dummy's Chest Deflections Due to Three- and Two-Point Belt Loadings." Under this Order, UMTRI has adapted the Hybrid III dummy's chest deflection characteristics to the MVMA2D crash victim simulation program and performed parametric studies to determine how chest deflection of two-point and three-point belt-restrained dummies are affected by belt properties, seat cushion geometry and stiffness, floor board and knee cushion locations.

DATA RESOURCES

Four information sources were used in developing the data sets for this study. The first of these was used to obtain vehicle interior geometric data. The Volkswagen Rabbit vehicle interior, occupant posture, H-point location, and two-point belt geometry were obtained from previous work conducted at UMTRI reported in "Biomechanical Accident Investigation Methodology." This report, authored by D. H. Robbins, J. W. Melvin, D. F. Huelke, and H. W. Sherman, was the output from a project sponsored by MVMA that was completed in 1983. The vehicle data were obtained from seating package drawings supplied by Volkswagen of America. They were used in the successful reconstruction of an offset head-on crash between a 1979 Blazer and a 1980 VW Rabbit. Both occupants of the Rabbit were wearing automatic shoulder belts.

The second data source was used to replace the human data used in the accident reconstruction with Hybrid III parameters. The source for the Hybrid III parameters in MVMA2D format was a data set provided by General Motors to NHTSA for general use.

The third data source was used to replace the vehicle deceleration estimated for the crash reconstruction mentioned above. The new barrier crash pulse that was used was obtained at TRC.

The fourth, and final, data source provided upgraded advanced three-dimensional belt geometry developed from concepts used in a recent study conducted for industry.

METHOD FOR DETERMINING CHEST DEFORMATION

Figures 1 and 2 show the geometry of the model which is used to estimate chest deflection from MVMA2D simulation output. Two configurations of the torso belt crossing the chest are shown in Figure 1. The first (solid line) is the path over the chest for the MVMA2D simulation. This reflects the fact that the belt is attached to points on the chest which cannot move with respect to the chest center of gravity. The second (dotted line) shows the path the belt would take over the torso if chest deflection is allowed. The displacement at the top of the chest is shown to be different from the displacement at the bottom. In order for dummy kinematics predicted by the MVMA2D model to match test data that includes Hybrid III chest deformation, it is necessary to reduce belt stiffness for the computer simulation to allow more belt stretch for the same applied force.

Figure 2 shows details of belt and chest deformation and the effect of applied forces on both. The upper and lower belts as well as the chest are shown as free bodies. Elongation of all belts includes the effects of the applied forces on the upper and lower sections. An additional elongation is included for the MVMA2D model simulation to take into account the effect of chest deflection. This additional elongation effect depends on both belt angle and the deflection at the top and bottom of the chest. The assumption has been made that the difference in belt angle is small between the MVMA2D and test conditions. Different stiffnesses have been assigned to the top and bottom of the chest to test the hypothesis that Hybrid III dummy chest deflection may have more than one degree of freedom (at a minimum, rotational as well as uniaxial motion).

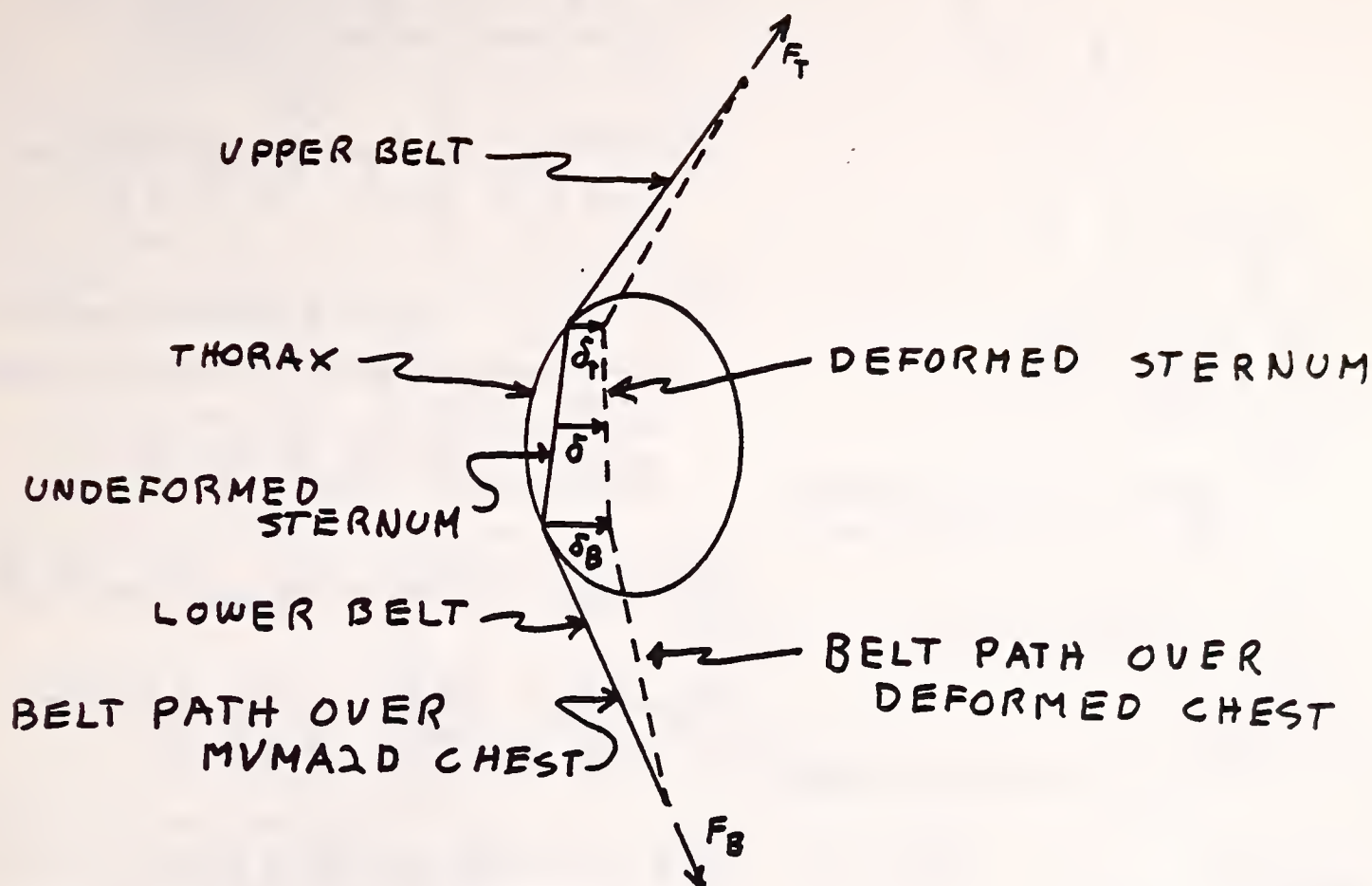
The geometric model that has been presented can now be used to develop a method for using the unmodified MVMA2D model to predict differential chest deflections. The first step is to make a major assumption that both belt and chest stiffnesses can be modeled by linear springs as is done in the following simplistic analysis. The belt force components normal to the chest are related to the displacements at its top, bottom, and center by the equations,

$$F_T \cos \theta_T = k_T \delta_T$$

$$F_B \cos \theta_B = k_B \delta_B$$

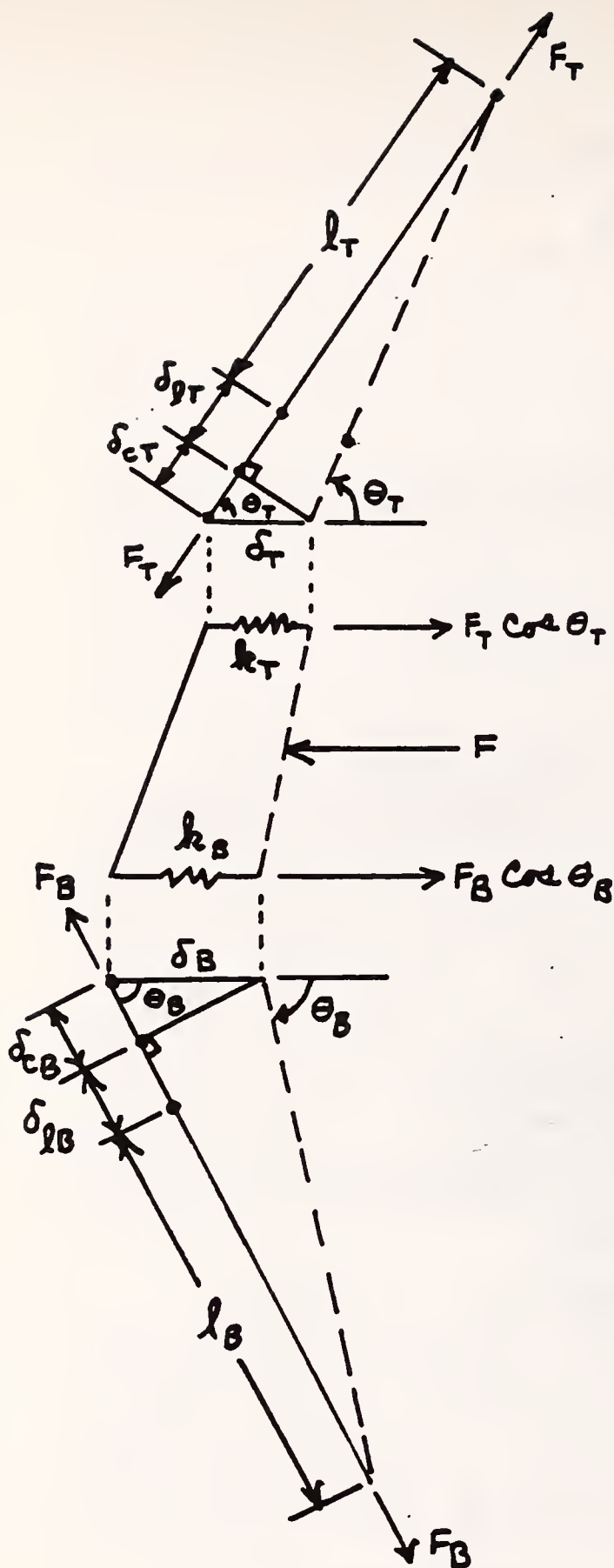
$$F = F_T \cos \theta_T + F_B \cos \theta_B$$

$$F = k_c \delta = k_T \delta_T + k_B \delta_B = k_c \left(\frac{\delta_T + \delta_B}{2} \right)$$



δ_T = deflection at top of sternum
 δ = mid-sternum deflection
 δ_B = deflection at bottom of sternum
 F_T = force in upper belt
 F_B = force in lower belt

Figure 1. Schematic of MVMA2D model of belt path over chest with effect of chest deformation superimposed.



l_T and l_B = unstretched length of upper and lower belts

δ_{l_T} and δ_{l_B} = elongation of belt due to belt force, F_T and F_B .

δ_{c_T} and δ_{c_B} = added belt elongation to account for chest compression within limits of MVMA 20 belt model (fixed to torso).

θ_T and θ_B = Belt angles with vertical

k_T and k_B = Stiffnesses at top and bottom of chest

F = overall reaction force of sternum to applied belt forces

δ_T and δ_B = deflections at top and bottom of chest.

F_T and F_B = Forces acting on upper and lower belt segments

Figure 2. Details of belt and chest deformation and the effects of the applied forces.

where h_c is the overall chest stiffness. If the compliances at the top and bottom of the chest are the same,

$$h_T = h_B = h$$

$$k_c \left(\frac{\delta_T + \delta_B}{2} \right) = h (\delta_T + \delta_B)$$

$$h_c = 2h$$

Note from Figure 2 that the MVMA2D belt elongation effect due to chest deflection can be expressed in terms of chest deflection as,

$$\delta_{cB} = \delta_B \cos \theta_B$$

$$\delta_{cT} = \delta_T \cos \theta_T$$

The force-deflection equations can now be written,

$$F_T \cos \theta_T = \frac{h_c}{2} \delta_T = \frac{h_c}{2} \frac{\delta_{cT}}{\cos \theta_T}$$

$$F_B \cos \theta_B = \frac{h_c}{2} \delta_B = \frac{h_c}{2} \frac{\delta_{cB}}{\cos \theta_B} \quad (1)$$

In terms of either belt force, or deflection in the belt, they can be rewritten as,

$$\delta_{cT} = \frac{2 \cos^2 \theta_T}{h_c} F_T \quad ; \quad \delta_{cB} = \frac{2 \cos^2 \theta_B}{h_c} F_B$$

$$F_T = \frac{h_c}{2 \cos^2 \theta_T} \delta_{cT} \quad ; \quad F_B = \frac{h_c}{2 \cos^2 \theta_B} \delta_{cB} \quad (2)$$

These simplistic equations illustrate the interacting effects of chest stiffness, belt angle, and belt properties for given belt forces. If belt angle is zero, then the entire belt force is applied to chest deformation. As the belt angle increases toward 90 degrees, the effect becomes less. Different belt angles at the top and bottom of the chest can clearly have a major effect on the loads that are applied to the chest and the chest deflections which result.

Equations 2 provide the information needed to compute the amount of strain that must be added to the MVMA2D belt lengths for inclusion of the effect of Hybrid III chest deflection.

$$F_T = \frac{h_c l_T}{2 \cos^2 \theta_T} \left(\frac{\delta_{cT}}{l_T} \right) = \frac{h_c l_T}{2 \cos^2 \theta_T} \epsilon_{cT}$$

$$F_B = \frac{h_c l_B}{2 \cos^2 \theta_B} \left(\frac{\delta_{cB}}{l_B} \right) = \frac{h_c l_B}{2 \cos^2 \theta_B} \epsilon_{cB} \quad (3)$$

These equations define belt stiffness adjustments that include effects of chest deflection, belt angle, and belt length. Belt angle and length are known from the test setup geometry. The equations are used to compute the effects of shared deflection between the belt and the chest for inclusion in the input data for the MVMA2D model (Cards 710 and 711, fields 8 and 9 to define the material names, and cards 704-709 to define material properties).

Chest stiffness is based on post-test dummy calibration thorax impact data from the TRC Volkswagen Rabbit barrier impact mentioned earlier. Assuming a linear force-deflection curve, the chest stiffness is about 418 pounds/inch (5413.8 newtons maximum resistive force and 6.39 centimeters maximum deflection from the test) until geometric restrictions to motion are generated. Because of the "clavicle", only a small amount of deflection at the top of the chest beyond about 2.2 inches can take place. At the bottom of the chest, bottoming out begins to occur at about 3.25 inches. Beyond the points at which bottoming out is assumed to occur, a stiffness value of 12750 pounds/inch is chosen on the basis of data obtained from industry sources. So, up to a point, the bottom of the chest is more compliant than the top.

Equations 1 can be rewritten for use in estimating chest deflections from MVMA2D model output.

$$\delta_T = \frac{2 \cos \theta_T}{k_c} F_T, \quad \delta_B = \frac{2 \cos \theta_B}{k_c} F_B \quad (4)$$

Belt angle, belt force, and chest stiffness are all known. Maximum values of belt angles and forces are obtained from the MVMA2D output while different chest stiffnesses are used for the top and bottom of the chest. A short program in BASIC was written to compute the deflections from the MVMA2D output.

A final comment should be made about an assumption made in this analysis which is clearly illustrated in Figure 2. The computations are based on forces and deflections normal to the surface of the chest. The drawing correctly shows a surface line of the chest which is not normal to either deflection or force. The results will be most accurate when the torso is essentially upright during the application of crash loads. The predictions using this analysis are intended to show performance trends rather than quantitative results. To determine the accuracy of the procedure, validation against experimental results will be required.

MATRIX OF COMPUTER RUNS

Parameter studies have been conducted to determine how chest deflection of two-point and three-point belt-restrained dummies are affected by belt properties, seat cushion geometry and stiffness, as well as floor board and knee bolster locations. The following variations to the baseline two-point and three-point belt data sets have been made:

- Knee bolster moved 2 inches toward the front of the vehicle. Knee bolster moved 1.85 inches toward the occupant to almost touch the knees.
- Toeboard moved 4 inches toward the front of the vehicle.
- Knee bolster moved 2 inches toward the front of the vehicle and toeboard moved 4 inches toward the front of the vehicle.
- Upper torso belt anchor moved 4 inches toward the rear of the vehicle.
- Lower torso belt anchor (lap belt in the case of the three-point belt) moved 4 inches toward the rear of the vehicle and moved 4 inches toward the front of the vehicle.
- Both upper and lower belt anchors moved 4 inches toward the rear of the vehicle
- Belt stiffness reduced by a factor of 0.5
- Seat cushion stiffness reduced by a factor of 0.5
- Seat cushion friction set to 1.0
- Belt slack increased to 3.5 inches

The baseline data sets are included as Appendices A and B at the end of this letter report.

SUMMARY OF RESULTS

Tables 1 through 4 are a summary of the results obtained from the computer runs. A total of 44 computer runs were made. The earliest and most time consuming were those conducted while assembling data from the various data resources discussed previously. A total of 26 computer runs are included in the tables. A coding for the various runs is given as follows:

- 2 Pt Base. The baseline run for the two-point passive belt system.
- Bols+2. The entire bolster structure is moved forward 2 inches.
- Bols-1.85. The entire bolster structure is moved to nearly touch the occupant's knees.
- UT Anch-4. The anchor in the vehicle for the upper torso belt is moved 4 inches to the rear.
- LT Anch-4. For the two-point belt, the anchor in the vehicle for the lower section of the torso belt is moved 4 inches to the rear. For the three-point belt, the anchor in the vehicle for the stalk is moved 4 inches to the rear.
- LT Anch+4. Same as above except anchor is moved toward the front of the vehicle.
- UT< A-4. Both belt anchors are moved 4 inches toward the rear of the vehicle.
- Belt K*.5. The belt stiffness curve is reduced by a factor of 0.5.
- Slack=3.5. Belt slack in the various segments is increased from 1 inch to 3.5 inches.
- Toebo(a)rd+4. The entire toeboard structure is moved 4 inches toward the front of the vehicle.
- SC K*.5. The seat cushion stiffness curve is reduced by a factor of 0.5.
- SC Fric=1. The seat cushion friction coefficient is increased from 0.2 to 1.0.
- Bol+2,TB+4. The bolster and toeboard are moved toward the front of the vehicle by 2 inches and 4 inches respectively.

Table 1. Summary of Hip Motion, Femur Load, Chest Deceleration, and Chest Deflection Output (Two-point belts).

Variation	Hip X (in)	Hip Z (in)	Femur load (lb)	Chest G's	Upper chest defl. (in)	Lower Chest defl. (in)
2 Pt Base	6.43	1.14	4114	55.7	2.53	3.33
Bols+2	8.43	0.50	4850	66.2	2.59	3.37
Bols-1.85	4.24	1.74	3188	50.9	2.48	3.31
UT Anch-4	6.43	1.17	4107	54.0	2.51	3.32
LT Anch-4	6.32	1.02	4074	56.3	2.54	3.37
LT Anch+4	6.56	1.25	4162	54.2	2.51	3.29
UT< A-4	6.32	1.05	4068	55.6	2.52	3.35
Belt K*.5	6.59	1.22	4179	50.0	2.44	3.30
Slack=3.5	6.67	1.23	4626	59.2	2.49	3.32
Toeboard+4	6.41	1.15	4157	55.6	2.53	3.33
SC K*.5	6.68	1.74	4210	56.2	2.53	3.34
SC Fric=1	5.91	1.24	4120	56.7	2.54	3.34
Bol+2, TB+4	8.34	0.47	4698	65.7	2.59	3.37

Table 2. Summary of Hip Motion, Femur Load, Chest Deceleration, and Chest Deflection Output (Three-point Belts).

Variation	Hip X (in)	Hip Z (in)	Femur load (lb)	Chest G's	Upper chest defl. (in)	Lower chest defl. (in)
3 Pt Base	5.62	2.10	3119	47.6	2.39	2.88
Bols+2	7.19	1.76	2850	59.4	2.46	3.26
Bols-1.85	3.86	2.35	2608	41.8	2.35	2.37
UT Anch-4	5.62	2.11	3108	47.8	2.39	2.76
LT Anch-4	5.20	2.09	2753	49.2	2.40	3.27
LT Anch+4	6.13	2.01	3581	48.0	2.38	1.94
UT< A-4	5.20	2.09	2744	49.9	2.40	3.26
Belt K*.5	6.06	1.78	3587	38.1	2.31	2.21
Slack=3.5	6.62	1.40	4215	47.6	2.33	2.71
Toeboard+4	5.60	2.11	3193	47.3	2.39	2.84
SC K=.5	5.66	2.75	3195	47.3	2.39	2.91
SC Fric=1	5.37	1.92	3307	51.4	2.40	2.92
Bol+2, TB+4	7.08	1.78	2908	59.1	2.45	3.26

Table 3. Summary of Belt Output (Two-point Belts).

Variation	Up Belt Load (pounds)	Up Belt Angle (degrees)	Lo Belt Load (pounds)	Lo Belt Angle (degrees)
2 Pt Base	2661	14.44	2022	51.71
Bols+2	3079	14.03	2340	50.51
Bols-1.85	2388	15.35	1815	53.19
UT Anch-4	2520	12.18	1915	51.82
LT Anch-4	2714	14.74	2062	44.90
LT Anch+4	2546	13.99	1935	59.92
UT< A-4	2569	12.38	1952	44.95
Belt K*.5	2059	13.42	1565	49.57
Slack=3.5	2372	12.78	1803	48.68
Toeboard+4	2658	14.44	2020	51.73
SC K*0.5	2676	15.48	2034	50.24
SC F=1.0	2716	13.95	2064	52.19
Bol+2, TB+4	3073	14.00	2335	50.58

Table 4. Summary of Belt Output (Three-point Belts).

Variation	Up Belt Load (pounds)	Up Belt Angle (degrees)	Lo Belt Load (pounds)	Lo Belt Angle (degrees)
3 Pt Base	1777	15.13	1351	61.79
Bols+2	2192	14.93	1666	61.32
Bols-1.85	1490	15.48	1133	62.30
UT Anch-4	1752	12.67	1331	62.62
LT Anch-4	1844	15.63	1402	54.33
LT Anch+4	1670	14.26	1269	70.20
UT< A-4	1815	13.02	1379	54.39
Belt K*0.5	1196	13.89	909	57.35
Slack=3.5	1379	12.38	1048	54.93
Toeboard+4	1771	15.13	1346	62.05
SC K*0.5	1767	16.05	1343	61.28
SC Fric=1.	1818	14.50	1382	61.99
Bol+2, TB+2	2160	14.92	1641	61.33

OBSERVATIONS

The following six output parameters were included in the results given in Tables 1 - 4:

- Hip motion
- Belt loads
- Chest deflection (top and bottom)
- Knee loads
- Belt angles
- Chest G's

Observations of the effects of the various parameter variations on these quantities follow.

1. Hip motion. The X-motion of the hip is the smallest when the bolster is positioned closest to the knees. Likewise, it is the largest when the bolster is located furthest away. Conversely, the Z-motion is greatest when the bolster is closest, and also, when the seat cushion is softest. The hip X-motion is greater for two-point systems than it is for three-point systems. The converse is true for Z-motion.

2. Belt loads. Torso belt loads are largest when the bolster is positioned the furthest from the knees. This is due to the fact that the chest begins to absorb energy before the knees. Torso belt loads are lower when the bolster is closest and when belt slack is greatest. The reason for improved performance with an increase in belt slack in this case is the improved phasing of loads applied to the torso and hip. The smallest loads are applied in the case of the smallest belt stiffness. Loads in the two-point belt systems are larger than those in the three-point belt system.

3. Chest deflections. Chest deflections are larger for the two-point belt systems than they are for the three-point belt systems at both the top and the bottom of the chest. Lower chest deflection values are similar to, or larger than, upper chest deflection values for three-point belt loading. This depends on bolster and lower belt anchor locations. Forward belt anchor locations and bolsters positioned close to the knees result in deflections at the bottom of the chest which are similar in value to those at the top of the chest. In all cases with the two-point belt system, the deflection at the bottom of the chest is significantly larger than that at the top. This effect is accentuated by the blocking effect of the clavicle structure in the Hybrid III against an increase of belt angle as the dummy moves forward.

4. Knee loads. Knee loads are significantly lower for the three-point belt systems because the belts absorb a significant portion of the crash loading on the occupant.

5. Belt angles. The significantly larger angle of the lower torso element in the two-point belt system results in a larger force component normal to the surface of the chest than is the case with the three-point belt systems.

6. Chest G-loading. Chest G's are larger for two-point belts. This reflects the larger loads which are applied. The lowest loads are for the case of belts with reduced stiffness properties. The largest loads occur when there is a time delay before the occupant interacts with the vehicle. In these cases, the bolster is further from the knees or there is slack in the belt system.

APPENDIX A

TWO-POINT BELT SYSTEM
BASELINE DATA SET

18

19

APPENDIX B

THREE-POINT BELT SYSTEM
BASELINE DATA SET

22

Listing of D01VW4 at 22:12:12 on FEB 4, 1988 for CCId=SWLN on UM

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118	FLOOR	2.	1.	0.	0.	0.	0.	402
119	INST. PANEL	2.	1.	0.	0.	0.	0.	402
120	BOLSTER	1.	2.	1.	0.	0.	0.	402
121	WINDSHIELD	1.	1.	1.	0.	0.	0.	402
122	CUSHION	1.	3.	1.	0.	0.	0.	402
123	SEATBACK	1.	2.	1.	0.	0.	0.	402
124	ROOF	1.	2.	1.	0.	0.	0.	402
125	STEERING WHEEL	1.	5.	1.	0.	0.	0.	402
126	MATFL	0.	0.	0.	1000.	2000.	2400.	403
127	MATDASH	0.	0.	0.	1000.	2000.	0.	403
128	MATBOL	0.	0.	0.	1000.	2000.	0.	403
129	MATWD	0.	0.	0.	1000.	2000.	0.	403
130	MATCH	0.	0.	0.	1000.	2000.	0.	403
131	MATSB	0.	0.	0.	1000.	2000.	0.	403
132	MATRF	0.	0.	0.	1000.	2000.	0.	403
133	MATSTW	0.	0.	0.	1000.	2000.	0.	403
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135	MATDASH	2.	0.	0.	0.	DASHSTAT	INERZ	404
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138	MATCH	2.	0.	0.	0.	CHSTAT	INERZ	404
139	MATSB	2.	0.	0.	0.	SBSTAT	INERZ	404
140	MATRF	2.	0.	0.	0.	RFSTAT	INERZ	404
141	MATSTW	2.	0.	0.	0.	STWSTAT	INERZ	404
142	FLGR	-1.	.2					405
143	FLGR	-1.	.2					406
144	DASHGR	-1.	.8					405
145	DASHGR	-1.	.08					406
146	BOLGR	-1.	.8					405
147	BOLGR	-1.	.08					406
148	WGR	-1.	.95					405
149	WGR	-1.	.01					406
150	CHGR	-1.	.1					405
151	CHGR	-1.	.85					406
152	SBGR	-1.	.1					405
153	SBGR	-1.	.85					406
154	RFGR	-1.	.5					405
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156	STWGR	-1.	.95					405
157	STWGR	-1.	.05					406
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159	OASHSTAT	-1.	441.24	-109.64	9.3813	0.17045		407
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162	WDSTAT	-1.	2000.					407
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173	STWSTAT	8.	750.					407
174	STWSTAT	10.	10000.					407

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Frobins, D

Hybrid II

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